

Solar wind

Dynamic model: spherical $V =$ radial outflow velocity

$$\rho v \frac{dv}{dr} = -\frac{dp}{dr} - \frac{\rho GM}{r^2}$$

$$\nabla \cdot \rho \vec{v} = 0 \Rightarrow r^2 \rho v = \text{const}$$

Eugene Parker
1958

$$\dot{M} = 4\pi r^2 \rho v = \text{mass loss rate (or mass accretion rate)}$$

need energy eqn: let's take $T = \text{const} \equiv$

b.c. let $r_0 =$ base of wind $\sim R_*$ for simplicity. not right but illustrates all of the key ideas
 $T_0 = T(r_0) = T(r)$
 $\rho_0 = \rho(r_0)$ etc.

Comments:

1. Model describes ^{spherical} isothermal steady outflow from $*$
 Eqns same if $v \rightarrow -v$

\therefore model also describes spherical steady accretion of matter by a point mass

"Bondi" accretion \rightarrow more later
 $\hookrightarrow 1952$

2. real winds more complicated

- high mass stars radiation pressure & line driven winds

- heating & accel. by waves (sound & MHD)
 impt. mean & other stars

\hookrightarrow need additional force in mom. eqn &

$T = \text{const}$
 $\hookrightarrow \rho T \frac{ds}{dt} =$ heating term energy eqn

- too simplistic:
 real solar wind
 matches
 photosphere
 $"r_0"$ & $"\rho_0"$
 a bit arbitrary

$$\frac{dp}{dr} = \frac{kT}{m} \frac{de}{dr} = c_s^2 \frac{de}{dr}$$

$$c_s^2 = \frac{kT}{m} = \text{isothermal sound speed} = \text{const.}$$

$$v \frac{dv}{dr} = -c_s^2 \frac{de}{dr} - \frac{GM}{r^2}$$

$$= -\frac{2}{r} - \frac{1}{v} \frac{dv}{dr} \quad \text{from mass cons.}$$

$$\frac{1}{v} \frac{dv}{dr} (v^2 - c_s^2) = \frac{2c_s^2}{r} - \frac{GM}{r^2}$$

isothermal wind/accretion eqn.

similar to nozzle eqn.

∃ special point where $v^2 = c_s^2$ called sonic point denote r_s

$$\text{at } r_s \quad \frac{2c_s^2}{r} = \frac{GM}{r^2}$$

or dv/dr blows up

i.e.,

$$r_s = \frac{GM}{2c_s^2}$$

location of sonic pt.

L'Hopital's rule shows that at $r=r_s$

Want

$$\left(\frac{dv}{dr} \right)_{r_s} = \pm \frac{2c_s^3}{GM}$$

symmetry of wind/accretion

wind eqn + $T = \text{const} = T_0$ + $\dot{M} = 4\pi r^2 v = \text{const}$
specify our soln.

Consider soln of eqn w/ varying $v_0 \equiv v(r_0)$

$r_0 =$ base of wind

\textcircled{PPA} shows topology of solns.

Focus on solns w/ $v_0 < c_s$ (physical) winds start nearly at rest

\exists 3 classes of solns.

~~X~~ # 6 on curve unphysical double valued

~~X~~ # 3 on curve $v < c_s \forall r$

\Rightarrow hydrostatic models should be reasonably accurate

whenever

$v \ll c_s$ hydrostatic equil. applies

$$\rho \frac{dv}{dr} = \rho \frac{dr}{dr} = \frac{\rho g}{r}$$

Note: these solns pass through $r = r_s$: have $\frac{dv}{dr} = 0$

(like node result)

still have $p(r \rightarrow \infty) \gg p_{ISM}$

pressure gradient accelerates flow until $v \rightarrow c_s$

\rightarrow 3. # 1 on curve flow smooth accelerates

L'Hopital's rule

$$\left. \frac{dv}{dr} \right|_{r_s} = \frac{\pm 2c_s^3}{1 - \beta}$$

through sonic point "transonic soln"

physical wind soln! flow continuous

MHD winds

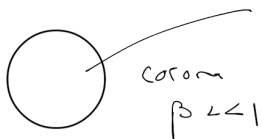
Rotating star.



In hydro $\dot{J} = \dot{M} R_*^2 \Omega$

$$\text{spinning time} = \frac{J}{\dot{J}} = \frac{M}{\dot{M}}$$

MHD fundamentally changes this



B-field tied to * & co-rotates

so long as $\beta^2 / 8\pi \gg \rho v^2, p_{gas}$

gas also co-rotates

\Rightarrow Δ mom of gas ϕ as it moves out

$$U\phi = R\Omega\phi \quad \& \quad \ell = R^2\Omega\phi$$

at expense of * rot KE & * mom

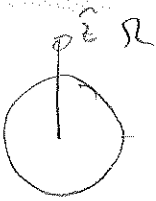
continues until outflow rot B dominated

$$\text{say } \rho v^2 \sim B^2 / 8\pi \quad (\text{Alfvén radius})$$

\Rightarrow outflow & B stresses remove far more
& mom. & rot- KE than in hydro

Key to * spindown, jets, & mom. transport in
dicks by large-scale B-fields

Full 3D theory hard: instead use "equatorial" wind the axisymmetry



look at outflow here

assume $V_\theta = 0, B_\theta = 0$

equatorial symmetry
 $\Rightarrow V_\theta = B_\theta = 0$

$$\vec{V} = V_r(r) \hat{r} + V_\phi(r) \hat{\phi}$$

rotation of $\hat{\phi} \rightarrow V_\phi$

$$\vec{B} = B_r(r) \hat{r} + B_\phi(r) \hat{\phi}$$

Basic eqs: mass, mom, induction, EOS

mass: $\rho V_r r^2 = \text{const}$

$$\nabla \cdot \vec{B} = 0 \Rightarrow r^2 B_r = \text{const}$$

induction $\frac{\partial \vec{B}}{\partial t} = \nabla \times (\nabla \times \vec{B})$

[see next page]

split monopole
 can't be true everywhere
 or else $\nabla \cdot \vec{B} \neq 0$
 monopole

$$\nabla \times (\nabla \times \vec{B}) = 0$$

$\vec{V} \times \vec{B}$ has no r, ϕ comp. only θ

writing out $\Rightarrow \frac{d}{dr} (r (V_r B_\phi - V_\phi B_r)) = 0$

set $V_r = 0$
 $B_\phi = 0$ or

$$V_\phi = rR$$

at "surface"

$$\text{use } B_r r^2 = B_\phi r^2$$

algebra \Rightarrow

$$\boxed{\frac{B_\phi}{B_r} = \frac{V_\phi - rR}{V_r}}$$

field freezing

int: solid body rotation $V_\phi = rR \Rightarrow B_\phi = 0$

field is radial & gas & field rotate together at R

in limit $r \rightarrow R \dots$

int:

$$\vec{V} = \alpha \vec{B} + r\Omega \hat{\phi}$$

$\vec{E} \times \vec{B}$ drift

$\alpha = \text{const}$

$$V_r = \alpha B_r$$

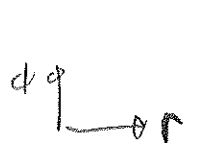
$$V_\phi = \alpha B_\phi + r\Omega$$

$$V_\phi = V_r \frac{B_\phi}{B_r} + r\Omega \Rightarrow$$

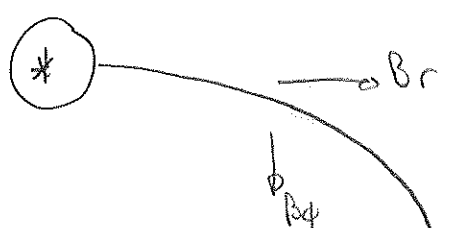
$$\frac{B_\phi}{B_r} = \frac{V_\phi - r\Omega}{V_r}$$

In inertial frame, \vec{B} is unchanging but gas rotates around w/ $r\Omega \hat{\phi} \rightarrow$ due to \vec{E} field & $\vec{E} \times \vec{B}$ drift. In addition to this particle can move along field lines freely ($\alpha \vec{B}$ part).

Notice solid body rotation $B_\phi = 0$ $V_\phi = r\Omega$
 corotating magnetosphere



$$V_\phi < r\Omega \quad B_\phi < 0$$



gas "lags behind" corotation & drags field w/ it \rightarrow get

mom eqn: $(\vec{v} \cdot \vec{v}) \vec{v} = -\nabla p - \frac{GM_* \vec{r}}{r^2} + \frac{1}{4\pi} (\nabla \times \vec{B}) \times \vec{B}$

B-force = $-\frac{1}{4\pi} \left(\frac{B_\phi}{r} \frac{d}{dr} (r B_\phi) \right) \vec{r} + \frac{1}{4\pi} \left(\frac{B_r}{r} \frac{d}{dr} (r B_\phi) \right) \vec{\phi}$

$\vec{B} = \vec{\nabla} \psi$
 $\approx B_r \frac{d}{dr} \psi + \frac{B_\phi}{r}$

\downarrow
 radial
 accel.
 pressure & tension

\downarrow
 \Rightarrow torque on
 outflow
 (mag. tension)

ϕ comp of momentum eqn. \rightarrow

$\rho v_r \frac{d}{dr} (r v_\phi) = \frac{B_r}{4\pi} \frac{d}{dr} (r B_\phi)$

\downarrow
 Lagrangian
 change in
 & mom.

\hookrightarrow B torque

mult. by r^2 & integrate $\rho r^2 v_r + r^2 B_r = \text{const.}$

\Rightarrow $L = r v_\phi - \frac{r B_r B_\phi}{4\pi \rho v_r} = \text{const.}$

$L =$ & mom. per unit mass carried by outflow

$L = L_{\text{gas}} + L_{\text{mag}}$

$\rightarrow B_\phi < 0$ so $L_{\text{mag}} >$

substitute in $\frac{B\phi}{Br} = \frac{U\phi - r\dot{\phi}}{U_r}$ into

$L \approx \text{const eqn} \Rightarrow$

gets rid of $B\phi$ in favor of Br

$$U\phi = r\Omega \left(\frac{\frac{U_r^2 L}{r^2 R} - V_{Ar}^2}{V_r^2 - V_{Ar}^2} \right)$$

$$V_{Ar}^2 = \frac{Br^2}{4\pi r}$$

Note: $V_{Ar} \propto \frac{Br}{r} \sim \frac{1}{r}$

as $r \rightarrow \infty$
 $Br \propto r^{-2}$
 $\propto r^{-2}$

as flow radially accelerated, passes through

critical pt. where $U_r = V_{Ar}$

Aifuen pt. radius $r = r_A$

smooth transition requires $N_{\text{Mach}} = 0$

$$\frac{U_r^2 L}{r^2 R} = V_{Ar}^2 \Rightarrow L = r_A^2 R$$

~~A momentum extracted from A as if gas corotates out to Aifuen pt.~~

~~in reality doesn't quite corotate out to r_A~~

~~but B stresses carry A momentum \rightarrow~~

w/ $L = r_A^2 \Omega$ in V_ϕ eqn.

$$V_\phi = r\Omega \left(\frac{V_r^2 \frac{r_A^2}{r^2} - V_{Ar}^2}{V_r^2 - V_{Ar}^2} \right)$$

2 limits

(2) $r \rightarrow \infty$ $V_{Ar} \rightarrow 0$
 $V_r \rightarrow \text{const}$

$\Rightarrow V_\phi \propto 1/r$ so, $l = rV_\phi = \text{const}$

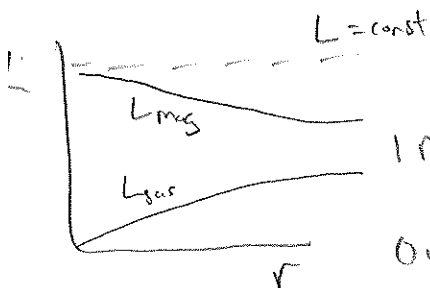
ϕ of gas conserved B weak
as $r \rightarrow \infty$
no torque

(1) $r \rightarrow r_A$ $V_r \rightarrow 0$

$V_\phi = r\Omega$ $\Omega = \text{const}$ Corotation

Impl.: $L = r_A^2 \Omega$

ϕ mom. removed
as $r \rightarrow \infty$ gas corotates
out to Altun pt.



In reality gas doesn't quite corotate
out to r_A but B stresses carry ϕ

mom. $\Rightarrow L = r_A^2 \Omega$ $\sim 2/3 - 1$
 \Rightarrow B stresses dominate $V_\phi = v_r(r \rightarrow \infty)$
 $\propto r^2 \Omega(r)$

Implication:

$$\dot{J} = \dot{M} L = \dot{M} R_A^2 R$$

$$\frac{R_A^2}{R_A^2}$$

larger than
hydro
model

$$\therefore \hat{T}_J = \text{spindown time} \approx \frac{J}{\dot{J}} = \frac{M R_A^2 R}{\dot{M} R_A^2 R}$$

$$\hat{T}_J \approx \frac{M}{\dot{M}} \frac{R_A^2}{R_A^2}$$

even if only a small amount of mass
lost large lever arm to $R_A \Rightarrow R_A$

\Rightarrow significant spindown

e.g. current ^{star} models have $R_A = 30 R_\odot$

$$\dot{M} \approx 2 \times 10^{-14} M_\odot \text{ yr}^{-1}$$

$$\Rightarrow \hat{T}_J \approx 5 \times 10^{10} \text{ years}$$

But for \dot{M} larger in past so that
spindown significant &
 \sim accounts for current rotation
of sun _{slow}

We've discussed in detail Σ mass & rotation of wind: what about energetics?

in hydro \exists conserved quantity

$$Be = \frac{1}{2}(v_r^2 + v_\phi^2) + h - \frac{GM_*}{r} \quad \text{enthalpy} = \frac{h}{\rho} \frac{kg}{m^3}$$

energy per unit mass flows in r direction

In MHD must worry about B transport of energy

Poynting Flux $\vec{S} = \frac{c}{4\pi} (\vec{E} \times \vec{B})$ energy per unit area per unit time

$$\vec{E} = -\frac{\vec{v} \times \vec{B}}{c} \Rightarrow \vec{S} = \vec{B} \times (\vec{v} \times \vec{B}) / 4\pi$$

$$\vec{S} = \frac{\nabla B^2}{4\pi} - \frac{\vec{B}(\vec{v} \cdot \vec{B})}{4\pi}$$

Subst. in for $\vec{v} \cdot \vec{B}$

$$\frac{v_\phi}{r} = \frac{B_\phi}{B_r} \dots$$

$$\Rightarrow \vec{S} = \underbrace{-\frac{r B_r B_\phi}{4\pi}}_{\text{key}} \vec{r} + \frac{r B_r^2}{4\pi} \hat{\phi}$$

conserved

\therefore In MHD \vec{r} radial energy flux is

$$F_r = (B_\phi)^2 r^2 v_r + r^2 S_r = \text{const.}$$

$$\therefore Be + \frac{S_r}{\rho v_r} = \text{const} \quad \text{since } r^2 \rho v_r = \text{const}$$

const.
0.005 /
per
unit
mass

$$\Sigma \equiv \underbrace{\frac{1}{a} (v_r^2 + v_\theta^2) + h - \frac{GM_*}{r}}_{\Sigma_{\text{gas}}} - \underbrace{\frac{rR B_\theta B_r}{4\pi r v r}}_{\Sigma_{\text{mag}}} = \text{const.}$$

$$\Sigma = \Sigma_{\text{gas}} + \Sigma_{\text{mag}}$$

$$L = L_{\text{gas}} + L_{\text{mag}} = r v \left(h - \frac{r B_r B_\theta}{4\pi r v r} \right)$$

$$\Sigma_{\text{mag}} = R L_{\text{mag}} \rightarrow \text{inlepp. energy is}$$

$$\dot{E} = \frac{1}{2} \dot{I} R^2 = \dot{I} R \dot{R}$$

$$\dot{I} = \dot{I} R \therefore \dot{E} = \dot{I} R \dot{I}$$

energetics of wind:

$$\text{hydro: } r \rightarrow 0 \quad \Sigma \approx h - \frac{GM_*}{r}$$

$$r \rightarrow \infty \quad \Sigma \approx \frac{1}{a} v r^2$$

energy comes from thermal energy of hot gas close to star

$$\text{MHD } \Sigma_{\text{mag}} = R L_{\text{mag}} \approx R_A^2 R^2 \quad \left(\text{fast bec. } L_{\text{mag}} \text{ not const.} \right)$$

2 kinds of MHD winds

$$h(R_*) \approx \frac{a^2}{R_*} \gg R_A^2 R^2 \Rightarrow \text{energetics same as hydro } \bar{E} \text{ impl. for spindown of } \bar{E} \text{ but wind thermally}$$

2. $R_A^2 R^2 \gg h$

magneto-centrifugal winds

energy ultimately
from rotational KE
of *



gas pressure irrelevant

wind accelerated by \vec{B} -field

transfer of Poynting flux
to bulk = KE

Solar wind firmly in class 1.

\vec{B} -field

cont. $\sim 1\%$ of final KE

(not necessarily
early in life, ...)

rapidly rotating stars, pulsars, jets from accretion disks

all class 2. energy from rotation mediated
by \vec{B} -field

We now und. basic dynamics — presy +
 a num — of MHD wind.

can calculate U_ϕ, B_ϕ given U_r

Lastly need eqn. for U_r

Derive as in hydro — radial mom. eqn can
 be manipulated $\Rightarrow \frac{dU_r}{dr} =$ algebraic no
 derivatives
 (sonic pt. eqn. in hydro)

for MHD wind, result is $a^2 = \frac{\gamma kT}{m}$

$$\frac{\Gamma}{U_r} \frac{dU_r}{dr} = \frac{(U_r^2 - U_{Ar}^2) (2a^2 + U_\phi^2 - \frac{GM_*}{r}) + 2U_r U_\phi U_{A\phi}}{(U_r^2 - U_{Ar}^2)(U_r^2 - a^2) - U_r^2 U_{A\phi}^2}$$

Den = 0 when

$$U_r^4 - U_r^2 (U_{Ar}^2 + U_{A\phi}^2) + U_{Ar}^2 a^2 = 0$$

2 solns:

$$U_r^2 = \frac{1}{2} (U_{Ar}^2 + U_{A\phi}^2) \left(1 \pm \left(1 - \frac{4U_{Ar}^2 a^2}{(U_{Ar}^2 + U_{A\phi}^2)^2} \right)^{1/2} \right)$$

$U_r^2 =$ radial phase speed
 of fast & slow
 magnetosonic
 waves

\Rightarrow 2 more critical pts. generalization of

Radiation Pressure Driven Winds

$$v \frac{dv}{dr} = -\frac{1}{\rho} \frac{dP_{\text{gas}}}{dr} + \frac{1}{c} k F = \frac{GM}{r^2}$$

$$\chi = \text{flux mean opacity}$$

$$= \frac{1}{F} \int \kappa_{\nu} F_{\nu} d\nu$$

$$F = L / 4\pi r^2 \quad \text{drop } P_{\text{gas}}$$

$$v \frac{dv}{dr} = \frac{\kappa L}{c \cdot 4\pi r^2} - \frac{GM}{r^2}$$

$$v \frac{dv}{dr} = \frac{\kappa}{c} \frac{1}{4\pi r^2} (L - L_{\text{Edd}})$$

$$4\pi r^2 \rho \times$$

$$\dot{M} \frac{dv}{dr} = \frac{\kappa \rho}{c} (L - L_{\text{Edd}})$$

$\tau =$ total
optical depth
through wind

$$\dot{M} v_{\infty} = \frac{\tau (L - L_{\text{Edd}})}{c} \approx \tau L / c$$

Note: momentum flux not limited to L/c
multiple scatterings

max τ is when all of the
photon energy is used to
accelerate the wind

$$\frac{1}{2} \dot{M} v_w^2 \approx \frac{\tau v_{\infty}}{2c} L \lesssim L$$

$$\tau_{\text{max}} \sim c / v_{\text{esc}}$$

"photon tired"

WR stars $\dot{M} v_w \sim 10^5 L/c$ observed
AGNs " in multiple scattering regime

Line Driven Winds

in hydrostatic situation, net opacity due to lines set by # of lines & thermal broadening

expanding wind this changes

$$l = \text{photon mfp} = 1/k\rho$$

$$\text{velocity difference across } l \approx \left| \frac{dv}{dr} \right| l$$

when $\left| \frac{dv}{dr} \right| l > v_{th}$ bulk Doppler shifts

enhance opacity by increasing line broadening

$$\tau \equiv \frac{v_{th}}{\left| \frac{dv}{dr} \right| l} = \frac{k_e \rho v_{th}}{\left| \frac{dv}{dr} \right|}$$

dimensionless measure of importance
of bulk optical depth

$\tau \ll 1$ large Doppler shifts

$$F_{rad} \equiv \frac{k_e F}{c} \overbrace{M(\tau)}^{\text{Force multiplier}}$$

often see $M(t) \equiv k t^{-\alpha}$

$$k \sim 0.1 - 1 \quad \alpha \sim 1/2$$

depending on * T_{eff}

LTB non-LTB

$$v \frac{dv}{dr} = -\frac{1}{e} \frac{dP_{SSS}}{dr} - \frac{GM}{r^2} + \frac{kF}{c} M(t)$$

$$t \equiv \frac{|x_e| e^{U_{th}}}{\frac{dv}{dr}}$$

critical pt. structure diff but

get wind solution via

analogous derivations